

1) Plane stress analysis

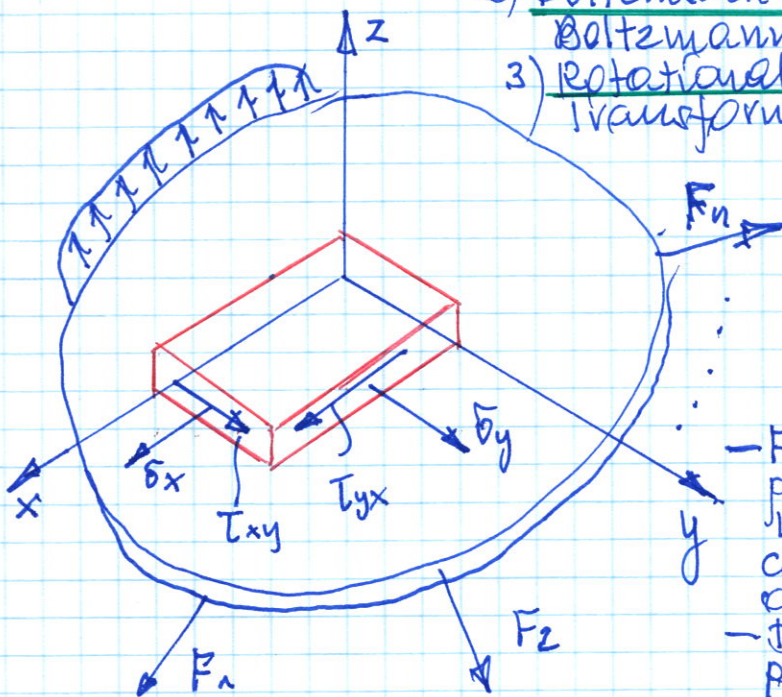
Analiza płaskiego stanu naprężenia

2) Boltzmann axiom. Postulat Boltzmann

3) Rotational transformation Transformacja obrotowa

4) Principal stresses Naprężenia główne

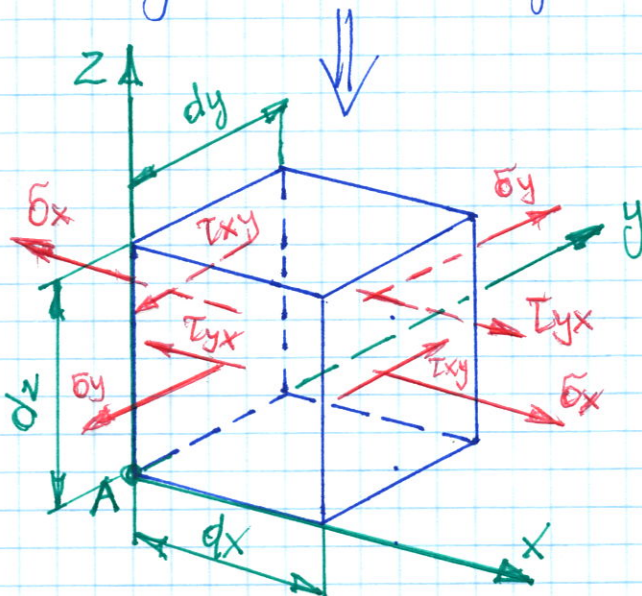
5) Mohr's circle Koło Mohra



— For any point A, three perpendicular sections were drawn. One section coincides with the plane of stress state

— Dla dowolnego punktu A poprowadzono trzy dowolnie prostopadłe przekroje. Jeden z nich pokrywa się z płaszczyzną stanu naprężenia

Principles of stress indexing
Zasady "indeksowania" naprężeń



— Infinitely close to point A, a second three of mutually perpendicular sections are drawn, respectively parallel to the previous three

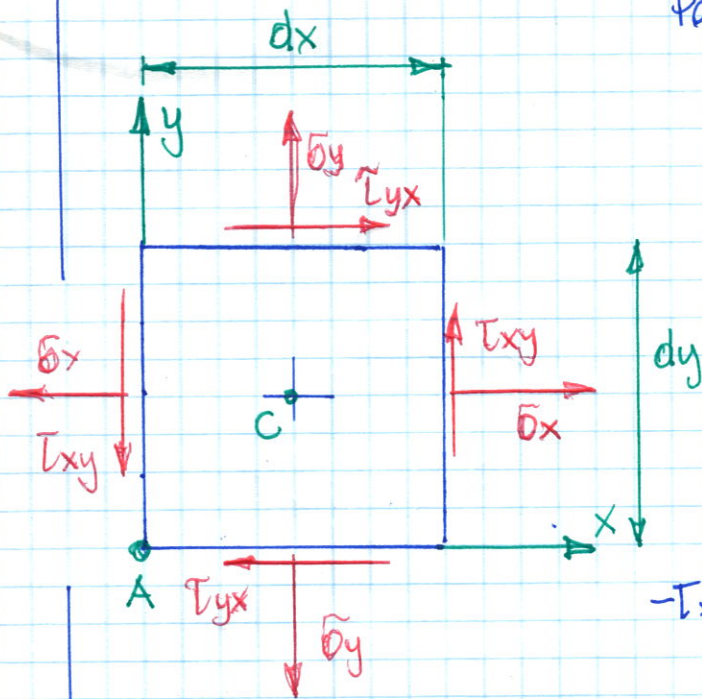
— Naśledzenie blisko punktu A poprowadzono drugą trójkę wzajemnie prostopadłych przekrojów, odpowiednio równoległych do poprzednich trójki

— A cuboid dx, dy, dz was created

— Otrzymano prostopadłościan

- If the body is in equilibrium, then the cuboid is in equilibrium (after applying stresses)
- Jeśli ciało jest w równowadze to i prostopadłościan jest w równowadze (po przyłożeniu naprężeń)

Boltzmann axiom
Postulat Boltzmanna



$$\sum M_i^C = -\tau_{xy} \cdot dy \cdot dz \cdot \frac{dx}{2} + \tau_{yx} \cdot dx \cdot dz \cdot \frac{dy}{2} - \tau_{xy} \cdot dy \cdot dz \cdot \frac{dx}{2} + \tau_{yx} \cdot dx \cdot dz \cdot \frac{dy}{2} = 0 \quad | : \frac{dx \cdot dy \cdot dz}{2}$$

$$\Downarrow$$

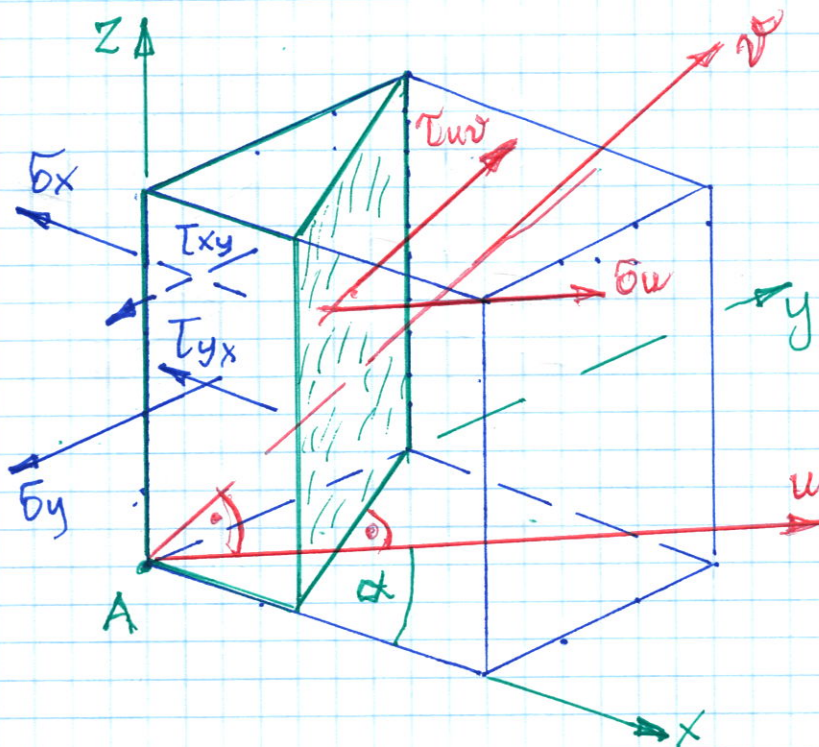
$$-\tau_{xy} + \tau_{yx} - \tau_{xy} + \tau_{yx} = 0$$

$$-2\tau_{xy} + 2\tau_{yx} = 0$$

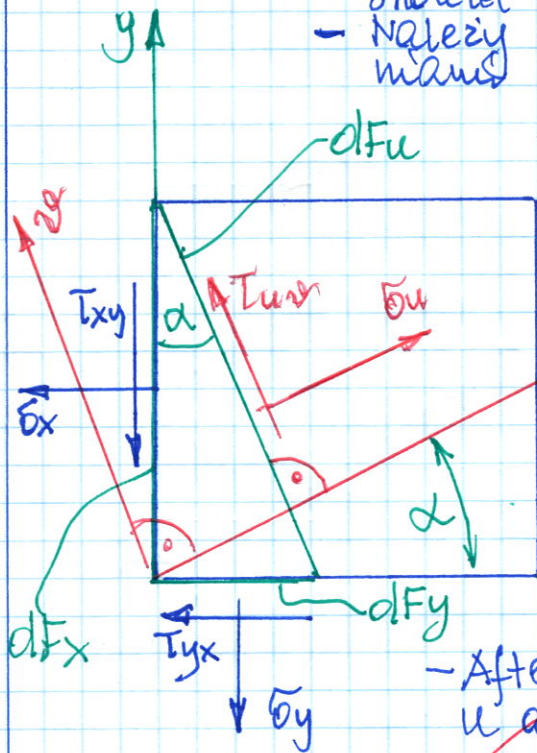
$$\boxed{\tau_{xy} = \tau_{yx}}$$

→ Stresses in diagonal section
Rotational transformation

— Naprężenia w przekroju ukośnym. Transformacja obrotowa



- Now the relationships between stresses should be considered
- Należy rozważyć związki między naprężeniami



- The cross-sectional areas perpendicular to the axes u, x, y , respectively, are marked as: dF_u, dF_x, dF_y

- Pola przekroju $\perp$ do osi u, x, y oznaczono odpowiednio jako: dF_u, dF_x, dF_y

- After the forces are projected on the u and v axes respectively

- Po zrzutowaniu sił na oś u oraz v odpowiednio:

$$dF_x = dF_u \cdot \cos \alpha, \quad dF_y = dF_u \cdot \sin \alpha$$

$$\textcircled{1} \sum P_{iu} = \sigma_u \cdot dF_u - \sigma_x \cdot dF_x \cdot \cos \alpha - \tau_{xy} \cdot dF_x \cdot \sin \alpha - \tau_{yx} \cdot dF_y \cdot \cos \alpha - \sigma_y \cdot dF_y \cdot \sin \alpha = 0$$

$$\textcircled{2} \sum P_{iv} = \tau_{uv} \cdot dF_u + \sigma_x \cdot dF_x \cdot \sin \alpha - \tau_{xy} \cdot dF_x \cdot \cos \alpha + \tau_{yx} \cdot dF_y \cdot \sin \alpha - \sigma_y \cdot dF_y \cdot \cos \alpha = 0$$

$$\textcircled{1} \sum F_{iu} = \sigma_u \cdot dF_u - \sigma_x \cdot dF_u \cos^2 \alpha - \tau_{xy} \cdot dF_u \cos \alpha \cdot \sin \alpha - \tau_{yx} \cdot dF_u \sin \alpha \cdot \cos \alpha - \sigma_y \cdot dF_u \sin^2 \alpha = 0 \quad | : dF_u$$

$$\textcircled{2} \sum F_{iv} = \tau_{uv} \cdot dF_u + \sigma_x \cdot dF_u \cos \alpha \cdot \sin \alpha - \tau_{xy} \cdot dF_u \cos^2 \alpha + \tau_{yx} \cdot dF_u \sin^2 \alpha - \sigma_y \cdot dF_u \sin \alpha \cdot \cos \alpha = 0 \quad | : dF_u$$

$$\text{from } \textcircled{1} \quad \sigma_u = \sigma_x \cdot \cos^2 \alpha + \sigma_y \cdot \sin^2 \alpha + 2 \tau_{xy} \cdot \sin \alpha \cdot \cos \alpha$$

$$\text{from } \textcircled{2} \quad \tau_{uv} = -(\sigma_x - \sigma_y) \sin \alpha \cdot \cos \alpha + \tau_{xy} (\cos^2 \alpha - \sin^2 \alpha)$$

ident / ale

$$\cos^2 \alpha = \frac{1 + \cos 2\alpha}{2}, \quad \sin^2 \alpha = \frac{1 - \cos 2\alpha}{2}$$

$$\sin \alpha \cdot \cos \alpha = \frac{\sin 2\alpha}{2}$$

$$\begin{aligned} \sigma_u &= \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\alpha + \tau_{xy} \sin 2\alpha \\ \tau_{uv} &= -\frac{\sigma_x - \sigma_y}{2} \sin 2\alpha + \tau_{xy} \cos 2\alpha \end{aligned}$$

for / gdy σ_v, τ_{vu}
for angle $= \alpha + 90^\circ$

$$\begin{aligned} \sigma_v &= \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos 2\alpha - \tau_{xy} \sin 2\alpha \\ \tau_{vu} &= \frac{\sigma_x - \sigma_y}{2} \sin 2\alpha - \tau_{xy} \cos 2\alpha \end{aligned}$$

$$\tau_{uv} = -\tau_{vu}$$

- find the extreme of the function for σ_u, τ_{uv} respectively
- wyznaczyć ekstremum funkcji odpowiednio dla σ_u, τ_{uv}

a) $\frac{d\sigma_u}{d\alpha} = 0 \Rightarrow \alpha = \alpha_0$ principal normal stress

$$-(\sigma_x - \sigma_y) \sin 2\alpha + 2\tau_{xy} \cos 2\alpha = 0$$

$$\left[\tan 2\alpha_0 = \frac{2\tau_{xy}}{\sigma_x - \sigma_y} \right] \Rightarrow \begin{aligned} \sigma_x &= \sigma_1 \\ \sigma_y &= \sigma_2 \\ \tau_{xy} &= 0 = \tau_{12} \end{aligned}$$

then / wówczas

$$\tau_{uv} = 0$$

When the extreme of the function σ_u , then $\tau_{uv} = 0$

$$b) \quad \frac{dT_{uv}}{d\alpha} = 0 \Rightarrow \alpha = \alpha_1$$

$$-(\sigma_x - \sigma_y) \cos 2\alpha - 2\tau_{xy} \sin 2\alpha = 0$$

$$\tan 2\alpha_1 = -\frac{\sigma_x - \sigma_y}{2\tau_{xy}}$$

$$\tan 2\alpha_1 = -\cot 2\alpha_0$$

$$\alpha_1 = \alpha_0 + \frac{\pi}{4}$$

principal
shear
stress

Rotational transformation (for principal stresses)
Transformacja obrotowa (dla naprężeń głównych)

$$\begin{aligned} \sigma_x &\Leftarrow \sigma_u = \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos 2\varphi \\ \sigma_y &\Leftarrow \sigma_v = \frac{\sigma_1 + \sigma_2}{2} - \frac{\sigma_1 - \sigma_2}{2} \cos 2\varphi \\ \tau_{xy} &\Leftarrow \tau_{uv} = -\frac{\sigma_1 - \sigma_2}{2} \sin 2\varphi \end{aligned}$$

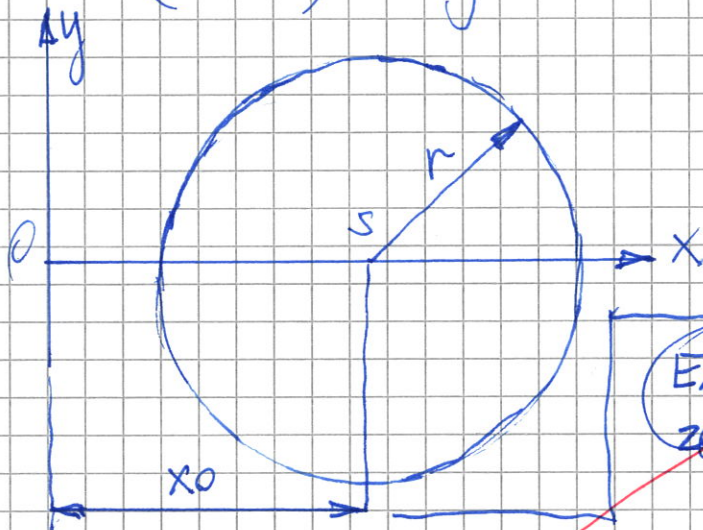
$$\begin{aligned} \sigma_1, \sigma_2, \tau_{12} &= 0 \\ \sigma_u, \sigma_v, \tau_{uv} &= ? \\ \downarrow \\ \sigma_x, \sigma_y, \tau_{xy} &= ? \end{aligned}$$

Mohr's circle (Otto Mohr)
Kóło Mohra

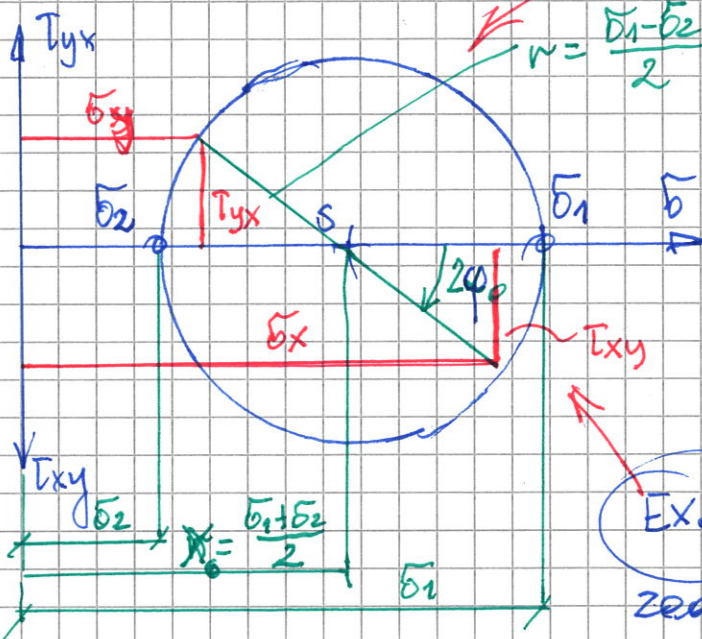
$$\begin{aligned} \left(\sigma_u - \frac{\sigma_1 + \sigma_2}{2} \right)^2 &= \left(\frac{\sigma_1 - \sigma_2}{2} \right)^2 \cos^2 2\varphi \\ \tau_{uv}^2 &= \left(\frac{\sigma_1 - \sigma_2}{2} \right)^2 \sin^2 2\varphi \end{aligned}$$

$$\begin{aligned} \left(\sigma_u - \frac{\sigma_1 + \sigma_2}{2} \right)^2 + \tau_{uv}^2 &= \left(\frac{\sigma_1 - \sigma_2}{2} \right)^2 \\ \left(\sigma_x - \frac{\sigma_1 + \sigma_2}{2} \right)^2 + \tau_{xy}^2 &= \left(\frac{\sigma_1 - \sigma_2}{2} \right)^2 \end{aligned}$$

$$(x - x_0)^2 + y^2 = r^2$$

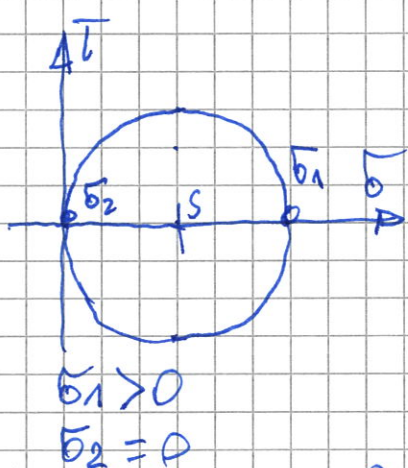


Exo 1. ϕ, σ_1, σ_2 ($\sigma_1 > \sigma_2$)
 zad. 1. $\sigma_x, \sigma_y, \tau_{xy} = ?$

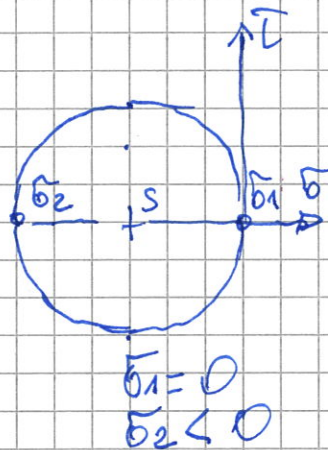


$$\left(\sigma - \frac{\sigma_1 + \sigma_2}{2} \right)^2 + \tau_{xy}^2 = \left(\frac{\sigma_1 - \sigma_2}{2} \right)^2$$

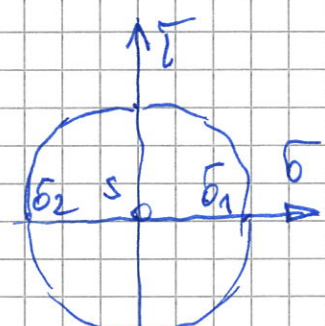
Exo 2. $\sigma_x, \sigma_y, \tau_{xy}$
 zad. 2. σ_1, σ_2, ϕ



$\sigma_1 > 0$
 $\sigma_2 = 0$
 (uniaxial tension)
 jednoosiowa rozciąganie



$\sigma_1 = 0$
 $\sigma_2 < 0$
 (uniaxial compression)
 jednoosiowe ściśnięcie



$\sigma_1 > 0$
 $\sigma_2 < 0$
 $|\sigma_1| = |\sigma_2|$

2

Homework / zadanie domowe

Exe 1. / zad. 1.

$$\sigma_1 = 600 \text{ MPa}, \quad \sigma_2 = -400 \text{ MPa}$$

$$\theta = 15^\circ$$

$\sigma_x, \sigma_y, \tau_{xy} - ?$
(analytically and graphically)

Exe 2. / zad. 2.

$$\sigma_x = 400 \text{ MPa}, \quad \sigma_y = -200 \text{ MPa}$$

$$\tau_{xy} = 300 \text{ MPa}$$

$$\sigma_1, \sigma_2, \alpha - ?$$

(analytically and graphically)